

TOPSS

Drainage Calculations

CITY OF OXFORD, BUTLER COUNTY, OH

FEBRUARY 28, 2025

PREPARED BY:

BAYER BECKER

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OXFORD, OHIO 45056

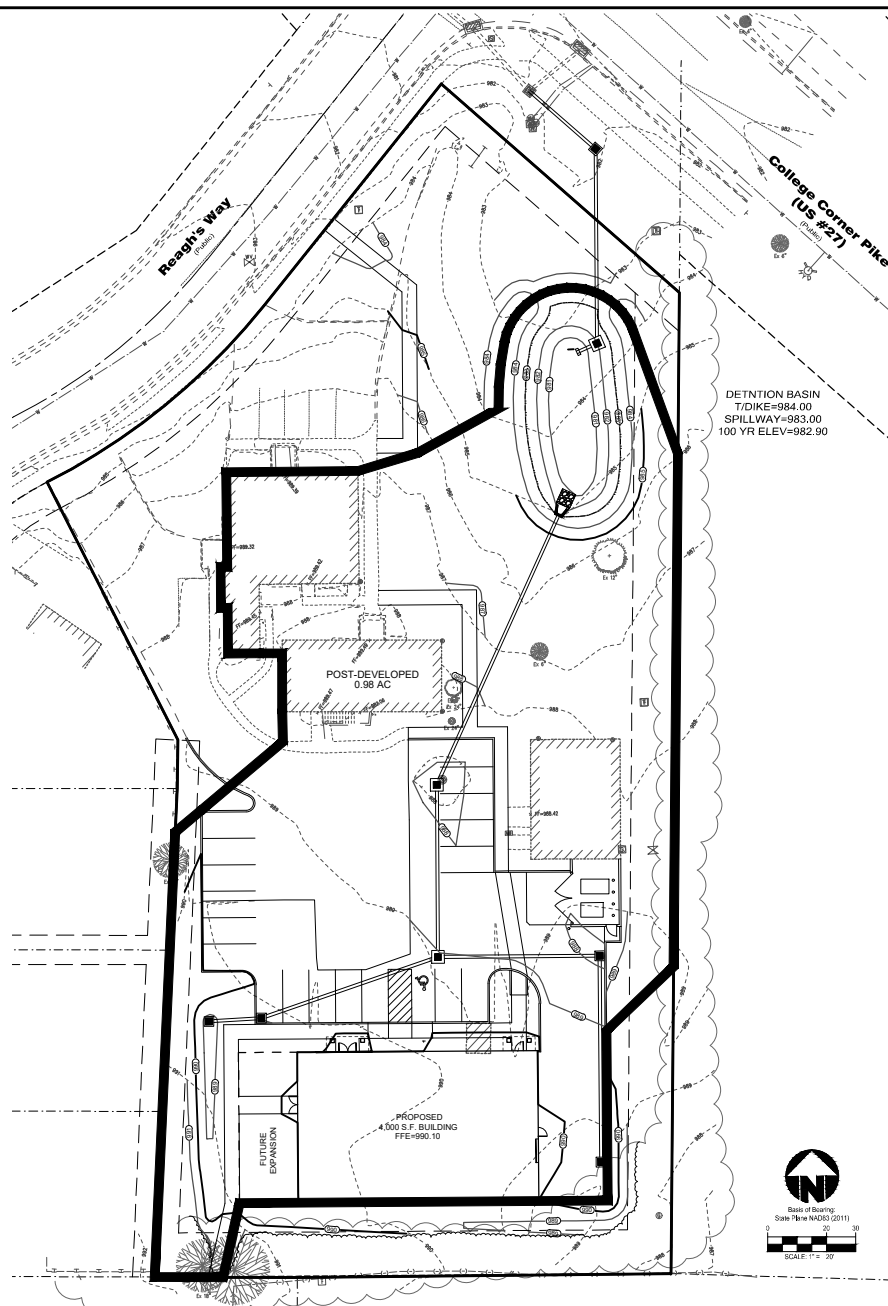
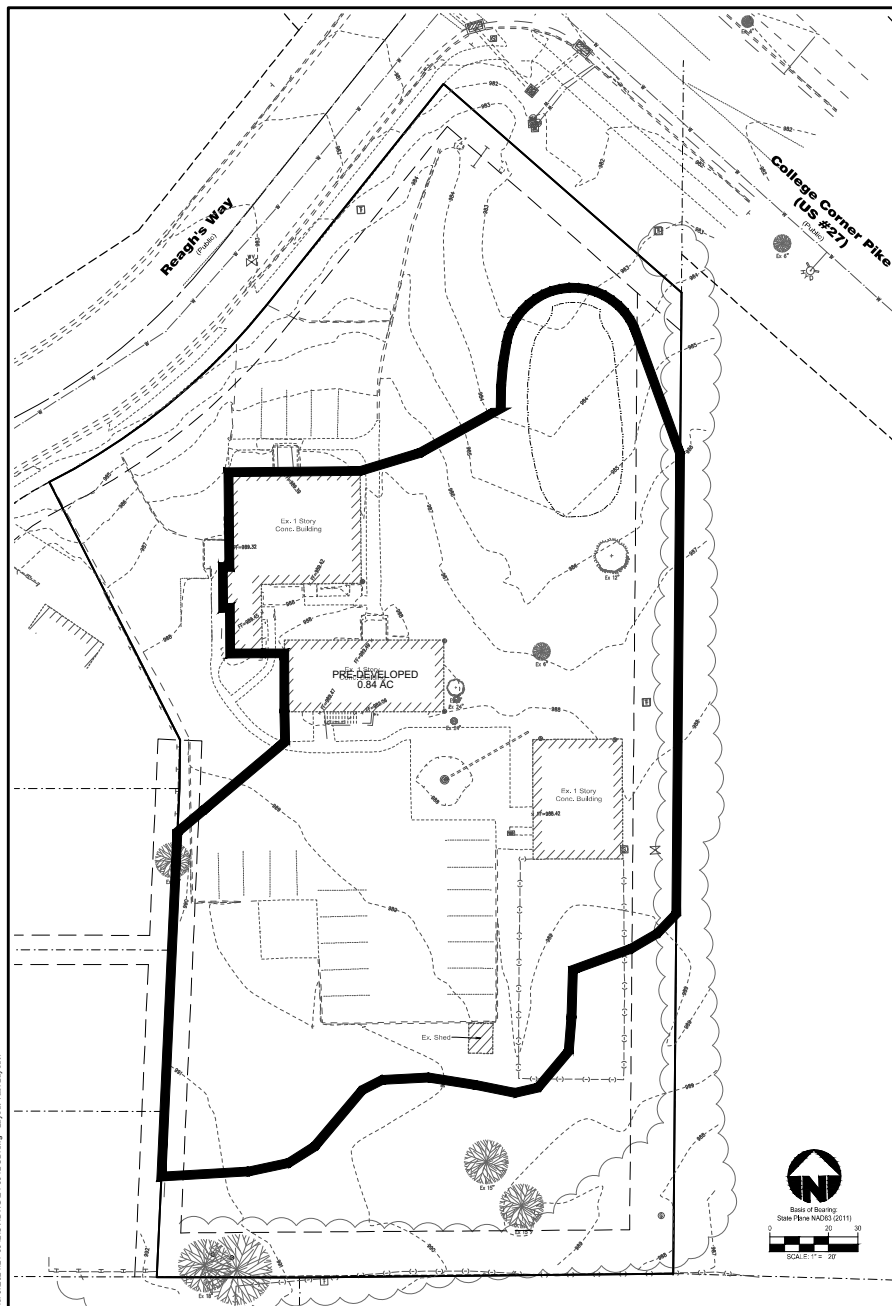
P (513) 523-4270

STORM WATER MANAGEMENT

TOPSS

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Hydrologic Soil Group—Butler County, Ohio











MAP LEGEND

Area of Interest (AOI)









 Area of Interest (AOI)

Soils

Soil Rating Polygons





 A
 A/D
 B
 B/D
 C
 C/D
 D
 Not rated or not available

Soil Rating Lines

 A
 A/D
 B
 B/D
 C
 C/D
 D
 Not rated or not available

Soil Rating Points






 A
 A/D
 B
 B/D

 C
 C/D
 D
 Not rated or not available

Water Features

 Streams and Canals

Transportation

 Rails
 Interstate Highways
 US Routes
 Major Roads
 Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Butler County, Ohio
 Survey Area Data: Version 24, Aug 27, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 19, 2022—Jun 21, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------|--------------|----------------|
| RxB | Russell-Urban land complex, gently sloping | C | 1.8 | 100.0% |
| Totals for Area of Interest | | | 1.8 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

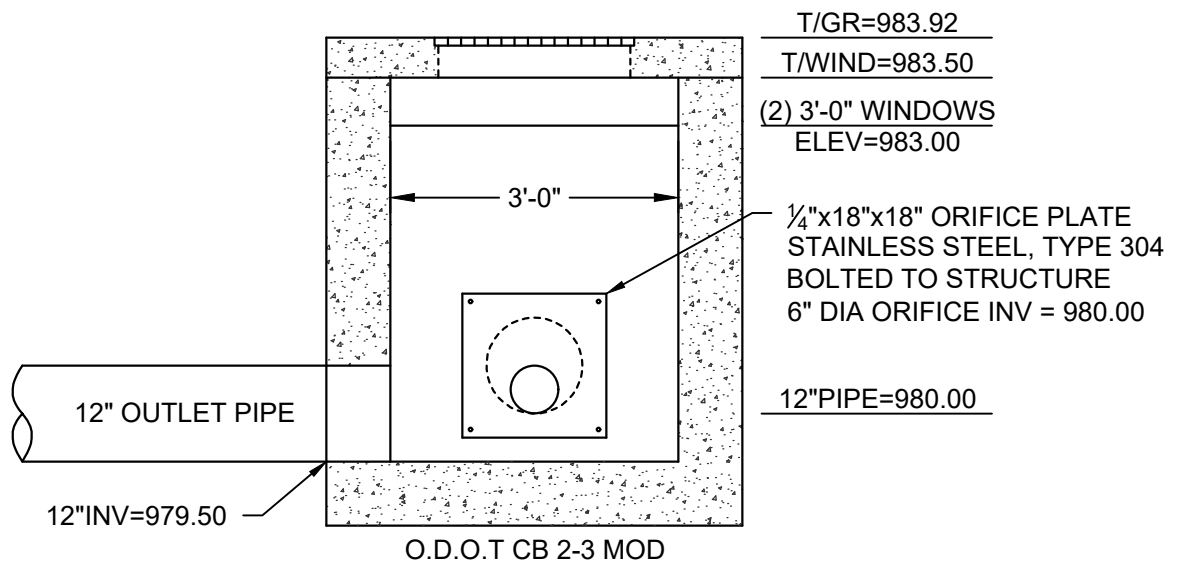
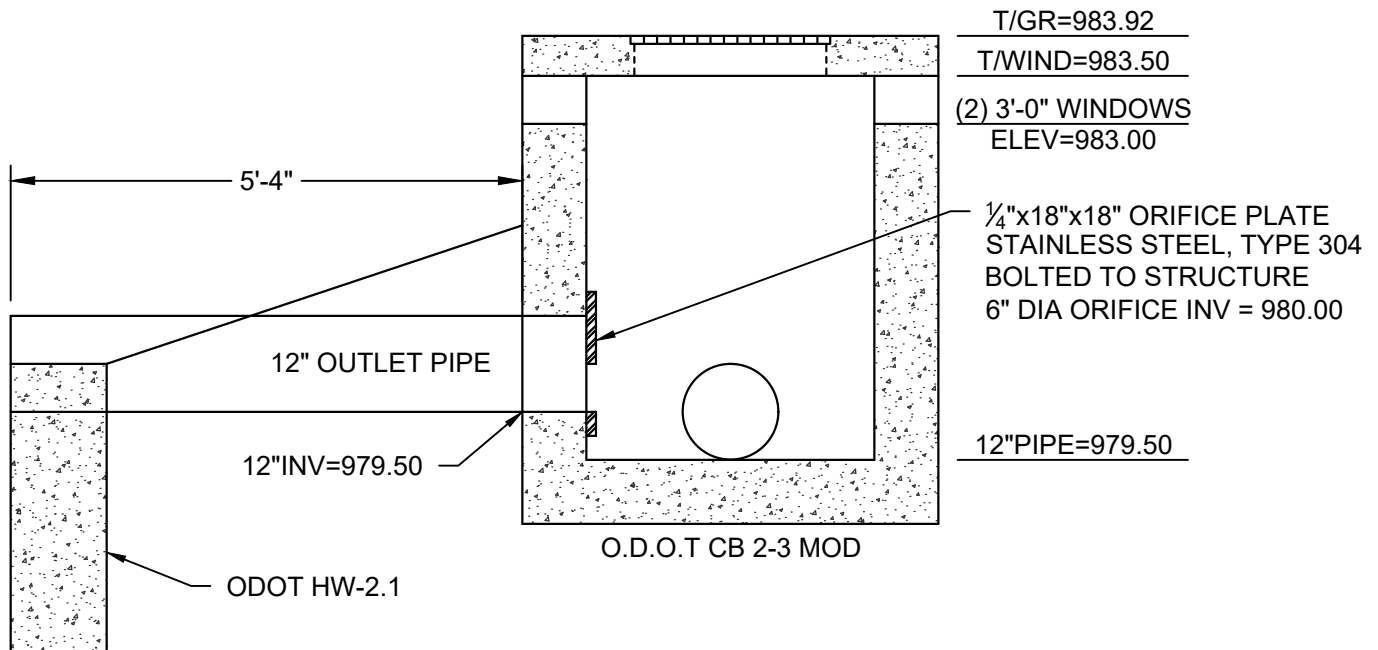
Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition



Drawing: 24-0042 CD
Scale: N.T.S.
Drawn by: GJK
Checked By:
Issue Date: 02-28-25

**TOPSS: TALAWANDA OXFORD
PANTRY & SOCIAL SERVICES**
SEC. 16, TOWN 5, RANGE 1, CONGRESS LANDS W. OF THE MIAMI
LOT 3285 OXFORD, BUTLER COUNTY, OHIO
5445 COLLEGE CORNER PIKE
OUTLET STRUCTURE DETAIL

**bayer
becker**
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110 S. College Avenue, Suite 101
Oxford, OH 45056 - 513.523.4270

DATE: 2-28-25

BY: GJK

CK'D:

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CIVIL ENGINEERING - SURVEYING
LANDSCAPE ARCHITECTURE - PLANNING

PROJECT: 24-0042

Storage Equation Method
Stormwater Detention Calculations

Pre Developed:

| <u>Description</u> | <u>Area</u> | <u>"c"</u> | <u>A x c</u> |
|--------------------|-------------|------------|--------------|
| Pervious | 0.52 | 0.30 | 0.16 |
| Impervious | 0.32 | 0.90 | 0.29 |
| | <u>0.84</u> | | <u>0.44</u> |

Weighted "c" = 0.53
Total Area = 0.84 Acres
 $T_c = 10$ Minutes

Post Developed:

| <u>Description</u> | <u>Area</u> | <u>"c"</u> | <u>A x c</u> |
|--------------------|-------------|------------|--------------|
| Pervious | 0.43 | 0.30 | 0.13 |
| Impervious | 0.54 | 0.90 | 0.49 |
| | <u>0.98</u> | | <u>0.62</u> |

Weighted "c" = 0.63
Total Area = 0.97 Acres
 $T_c = 10$ Minutes

Pre-Developed Intensities

(From Exhibit V-1, Page 115 City of Oxford, Stormwater Management Design Manual)

$I_1 = 3.07$ in/hr
 $I_2 = 4.08$ in/hr
 $I_5 = 4.85$ in/hr
 $I_{10} = 5.45$ in/hr
 $I_{25} = 6.30$ in/hr
 $I_{50} = 7.02$ in/hr
 $I_{100} = 7.69$ in/hr

Post-Developed Intensities

$I_1 = 3.07$ in/hr
 $I_2 = 4.08$ in/hr
 $I_5 = 4.85$ in/hr
 $I_{10} = 5.45$ in/hr
 $I_{25} = 6.30$ in/hr
 $I_{50} = 7.02$ in/hr
 $I_{100} = 7.69$ in/hr

Pre-Developed Runoff

$$Q_x = C I_x A$$

$Q_1 = 1.36$ cfs
 $Q_2 = 1.81$ cfs
 $Q_5 = 2.15$ cfs
 $Q_{10} = 2.42$ cfs
 $Q_{25} = 2.80$ cfs
 $Q_{50} = 3.12$ cfs
 $Q_{100} = 3.41$ cfs

Post-Developed Runoff

$Q_1 = 1.87$ cfs
 $Q_2 = 2.48$ cfs
 $Q_5 = 2.95$ cfs
 $Q_{10} = 3.32$ cfs
 $Q_{25} = 3.83$ cfs
 $Q_{50} = 4.27$ cfs
 $Q_{100} = 4.68$ cfs

Required Storage Volume, S_{100}

$$S_{100} = (Q_{100\text{post}} - Q_{100\text{pre}}) \times 30 \times 60 \text{ sec/min} = 2,280 \text{ Cu. Ft.}$$

Required Storage Volume per Frequency Event, S_x

$S_1 = 910$ Cu. Ft.
 $S_2 = 1,210$ Cu. Ft.
 $S_5 = 1,438$ Cu. Ft.
 $S_{10} = 1,616$ Cu. Ft.
 $S_{25} = 1,868$ Cu. Ft.
 $S_{50} = 2,081$ Cu. Ft.
 $S_{100} = 2,280$ Cu. Ft.

DATE: 2-28-25

BY: GJK

CK'D:

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LANDSCAPE ARCHITECTURE - PLANNING

PROJECT: 24-0042

**Storage Equation Method
Stormwater Detention Calculations**

Water Quality Volume Required = - Cu. Ft.
(Under 1.0 Acre disturbance - No Water Quantity Required)

Proposed Release Rates: From Hydraflow Pond Report

| Storm Event (Year) | Required Storage Volume (Cu. Ft.) | Total Required Volume (Cu. Ft.) | Provided Volume (Cu. Ft.) | Allowable Release Rate (cfs) | Basin Release Rate (cfs) | Total Post Release Rate (cfs) | Storage Elevation (ft) |
|--------------------------|--|--|---------------------------------|---------------------------------------|-----------------------------------|--|------------------------------|
| 1 | 910 | 910 | 1,083 | 1.36 | 1.25 | 1.25 | 982.00 |
| 2 | 1,210 | 1,210 | 1,362 | 1.81 | 1.32 | 1.32 | 982.20 |
| 5 | 1,438 | 1,438 | 1,642 | 2.15 | 1.39 | 1.39 | 982.40 |
| 10 | 1,616 | 1,616 | 1,781 | 2.42 | 1.42 | 1.42 | 982.50 |
| 25 | 1,868 | 1,868 | 2,060 | 2.80 | 1.48 | 1.48 | 982.70 |
| 50 | 2,081 | 2,081 | 2,339 | 3.12 | 1.54 | 1.54 | 982.90 |
| 100 | 2,280 | 2,280 | 2,479 | 3.41 | 1.57 | 1.57 | 983.00 |
| Max. | | | 4,489 | | 1.83 | | 984.00 |

| Spillway | |
|--------------------------|--------|
| Design Discharge (cfs)** | 3.41 |
| Spillway Invert | 983.00 |
| Spillway Length | 20.00 |
| Top of Dike Elevation | 984.00 |
| Flow Depth (ft) [C=2.6] | 0.16 |
| Freeboard | 0.84 |
| Spillway Side Slope | 4:1 |
| Velocity | 1.05 |

**Pre-Developed 100yr Discharge

Pond Report

Pond No. 1 - Detention Basin

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 980.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 980.00 | 00 | 0 | 0 |
| 1.00 | 981.00 | 641 | 214 | 214 |
| 2.00 | 982.00 | 1,121 | 870 | 1,083 |
| 3.00 | 983.00 | 1,689 | 1,395 | 2,479 |
| 4.00 | 984.00 | 2,350 | 2,010 | 4,489 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [PrfRsr] |
|-----------------|----------|--------|------|----------|
| Rise (in) | = 12.00 | 6.00 | 0.00 | 0.00 |
| Span (in) | = 12.00 | 6.00 | 0.00 | 0.00 |
| No. Barrels | = 1 | 1 | 0 | 0 |
| Invert El. (ft) | = 979.50 | 980.00 | 0.00 | 0.00 |
| Length (ft) | = 66.00 | 0.00 | 0.00 | 0.00 |
| Slope (%) | = 2.90 | 0.00 | 0.00 | n/a |
| N-Value | = .013 | .013 | .013 | n/a |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 |
| Multi-Stage | = n/a | Yes | No | No |

Weir Structures

| | [A] | [B] | [C] | [D] |
|----------------|----------------------|------|------|------|
| Crest Len (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| Crest El. (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Weir Type | = --- | --- | --- | --- |
| Multi-Stage | = No | No | No | No |
| Exfil.(in/hr) | = 0.000 (by Contour) | | | |
| TW Elev. (ft) | = 0.00 | | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|----------|--------------|--------------|-----------|-----------|-----------|------------|----------|----------|----------|----------|-----------|----------|-----------|
| 0.00 | 0 | 980.00 | 0.00 | 0.00 | --- | --- | --- | --- | --- | --- | --- | --- | 0.000 |
| 0.10 | 21 | 980.10 | 0.95 ic | 0.03 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.031 |
| 0.20 | 43 | 980.20 | 0.95 ic | 0.11 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.114 |
| 0.30 | 64 | 980.30 | 0.95 ic | 0.23 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.230 |
| 0.40 | 85 | 980.40 | 0.95 ic | 0.36 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.363 |
| 0.50 | 107 | 980.50 | 0.95 ic | 0.47 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.473 |
| 0.60 | 128 | 980.60 | 0.95 ic | 0.56 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.559 |
| 0.70 | 150 | 980.70 | 0.95 ic | 0.63 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.634 |
| 0.80 | 171 | 980.80 | 0.95 ic | 0.70 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.701 |
| 0.90 | 192 | 980.90 | 0.95 ic | 0.76 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.762 |
| 1.00 | 214 | 981.00 | 0.95 ic | 0.82 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.819 |
| 1.10 | 301 | 981.10 | 0.95 ic | 0.87 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.872 |
| 1.20 | 388 | 981.20 | 0.95 ic | 0.92 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.921 |
| 1.30 | 475 | 981.30 | 0.95 ic | 0.97 ic | --- | --- | --- | --- | --- | --- | --- | --- | 0.969 |
| 1.40 | 562 | 981.40 | 1.02 ic | 1.01 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.014 |
| 1.50 | 649 | 981.50 | 1.07 ic | 1.06 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.057 |
| 1.60 | 736 | 981.60 | 1.10 ic | 1.10 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.098 |
| 1.70 | 823 | 981.70 | 1.15 ic | 1.14 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.138 |
| 1.80 | 909 | 981.80 | 1.18 ic | 1.18 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.177 |
| 1.90 | 996 | 981.90 | 1.21 ic | 1.21 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.214 |
| 2.00 | 1,083 | 982.00 | 1.27 ic | 1.25 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.251 |
| 2.10 | 1,223 | 982.10 | 1.29 ic | 1.29 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.286 |
| 2.20 | 1,362 | 982.20 | 1.32 ic | 1.32 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.320 |
| 2.30 | 1,502 | 982.30 | 1.35 ic | 1.35 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.353 |
| 2.40 | 1,642 | 982.40 | 1.39 ic | 1.39 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.386 |
| 2.50 | 1,781 | 982.50 | 1.44 ic | 1.42 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.418 |
| 2.60 | 1,921 | 982.60 | 1.46 ic | 1.45 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.449 |
| 2.70 | 2,060 | 982.70 | 1.49 ic | 1.48 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.480 |
| 2.80 | 2,200 | 982.80 | 1.52 ic | 1.51 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.509 |
| 2.90 | 2,339 | 982.90 | 1.55 ic | 1.54 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.539 |
| 3.00 | 2,479 | 983.00 | 1.58 ic | 1.57 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.568 |
| 3.10 | 2,680 | 983.10 | 1.60 ic | 1.60 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.596 |
| 3.20 | 2,881 | 983.20 | 1.63 ic | 1.62 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.624 |
| 3.30 | 3,082 | 983.30 | 1.66 ic | 1.65 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.651 |
| 3.40 | 3,283 | 983.40 | 1.69 ic | 1.68 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.678 |
| 3.50 | 3,484 | 983.50 | 1.71 ic | 1.70 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.704 |
| 3.60 | 3,685 | 983.60 | 1.74 ic | 1.73 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.730 |
| 3.70 | 3,886 | 983.70 | 1.77 ic | 1.76 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.756 |

Continues on next page...

Detention Basin

Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 3.80 | 4,087 | 983.80 | 1.79 ic | 1.78 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.781 |
| 3.90 | 4,288 | 983.90 | 1.82 ic | 1.81 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.806 |
| 4.00 | 4,489 | 984.00 | 1.85 ic | 1.83 ic | --- | --- | --- | --- | --- | --- | --- | --- | 1.831 |

...End

(513) 336-6600

Project Name: TOPSS Pantry, 5445 College Corner Pike

$$Q_r = AC * I \text{ (required)}$$
$$V_p = (1.486 / n) * R^{2/3} * S^{1/2}$$
$$Q_p = A_p * V_p$$

Designed By: GJK
Reviewed By:
Date: 2/28/2025
Revised date:
Revised date:
Job # 24-0042

1

